

Ignition of Gaseous Methane/Oxygen Coaxial Mixtures

J. Sender, C. Pauli, M. Oschwald

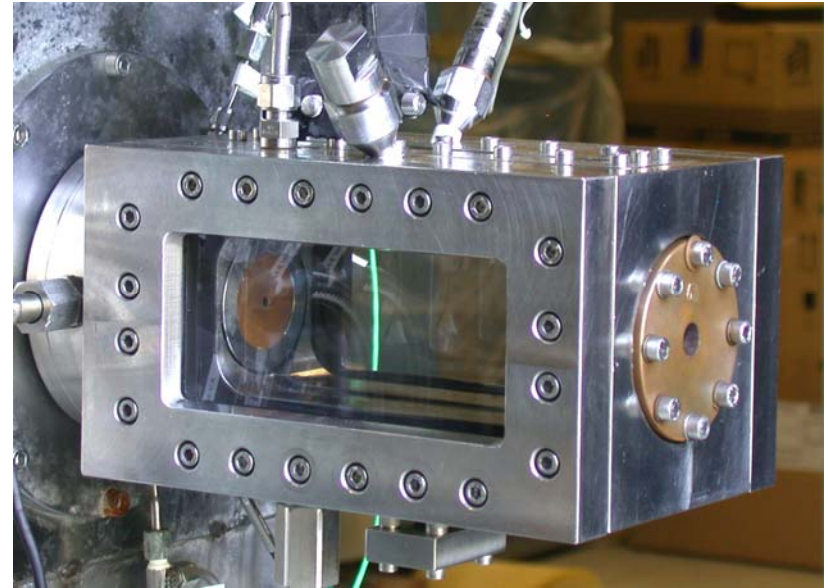
DLR Lampoldshausen



Deutsches Zentrum
für Luft- und Raumfahrt e.V.
in der Helmholtz-Gemeinschaft

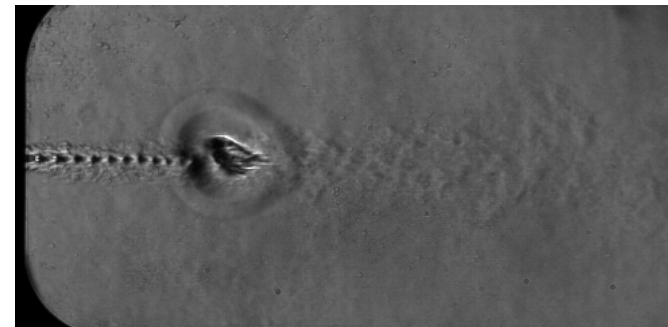
Contents

- Motivation
- Experimental setup & Test Conditions
- CH_4/O_2 Ignition phenomenology
- Mass flow rate effects
- Flame Stabilization
- Flame Anchoring - Influence of V & J ratios
- Conclusion



Motivation

- Ignition is still an issue for liquid propellant engines...reignition capabilities, etc.
- Goal : understand the ignition process to guarantee a reliable ignition
- Require: Focused experimental investigations on which to base specific CFD simulations

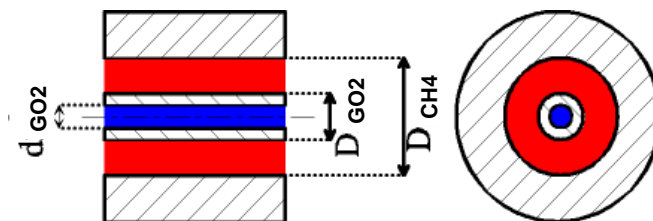
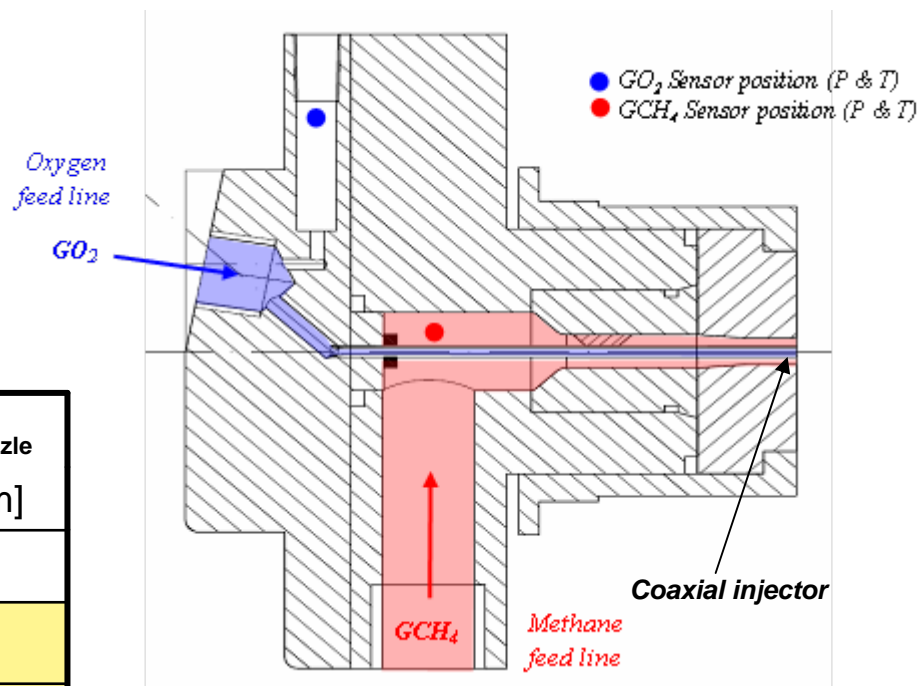


Experimental Setup (1)

Geometry

- Simple coaxial injector
- Four different injection configurations
- Test duration: 1 second

Test case	d_{GO_2} [mm]	D_{GO_2} [mm]	D_{CH_4} [mm]	D_{nozzle} [mm]
Case A	1.6	2.4	4.0	6
Case B	2.5	3.3	4.3	6
Case C1	2.5	3.3	3.6	6
Case C2	2.5	3.3	3.6	4
Case D	2.5	3.3	4.0	6



Experimental Setup (2)

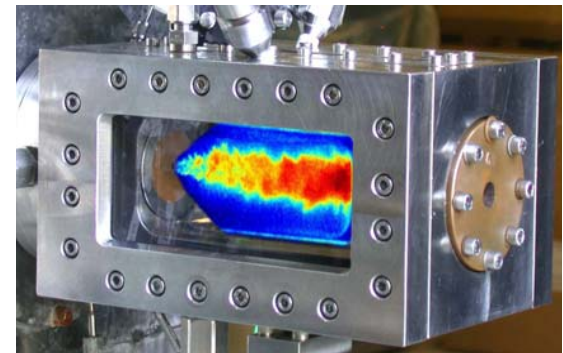
Injection conditions

Test case	Chamber Pressure P_c [bar]	Total mass flow \dot{m}_{tot} [g/s]	Mixture ratio ROF [-]	Methane velocity V_{CH_4} [m/s]	Oxygen velocity V_{GO_2} [m/s]	J [-]	V_{ratio} [-]
Case A	1.5	3.1	3.4	101	304	0.02	0.33
Case B	1.5 to 3.6	3.1 to 5.9	3.4	126	228	0.13	0.54
Case C1	2.3	4.6	3.4	412	239	1.53	1.72
Case C2	2.3	2.1	3.4	221	127	1.56	1.74
Case D	2.3	4.6	3.3	185	229	0.30	0.81

➤ Momentum flux ratio J : $J = \frac{\rho_{CH_4} u_{CH_4}^2}{\rho_{GO_2} u_{GO_2}^2}$

➤ Mixture ratio ROF: $r_{of} = \frac{\dot{m}_{GO_2}}{\dot{m}_{CH_4}}$

➤ Velocity ratio : $V_{ratio} = \frac{v_{CH_4}}{v_{GO_2}}$



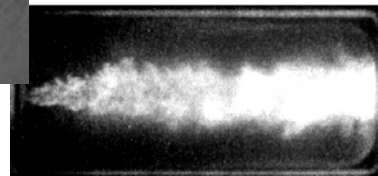
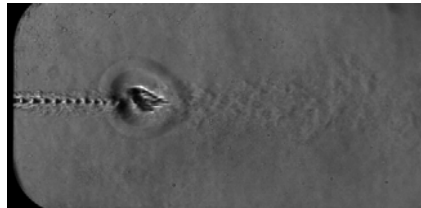
More than 100 tests performed

Experimental Setup (3)

➤ Laser Ignition

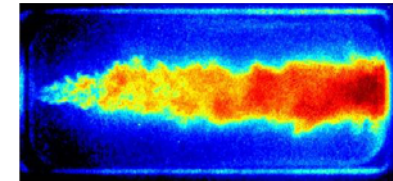
- Energy release in a specific volume by a focused laser beam
- Less representative than with an igniter, but:
 - Results in a well localized plasma (with high temperatures $\sim 10^6$ K) \rightarrow Position of initial flame kernel precisely known
 - Exact control of the ignition time to notably trigger the optical set up (Precision: ± 10 μ s)

Laser Type	Freq. doubled Nd:YAG
Wavelength	532 nm
Pulse Length	10 ns
Pulse Energy	95 mJ

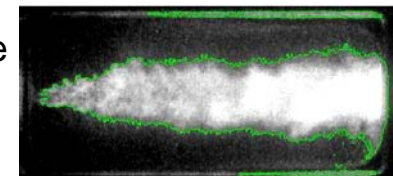


Raw Image

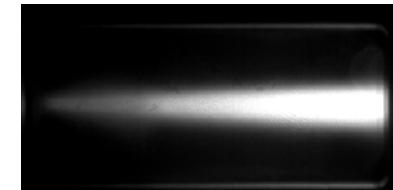
False color
➤



Flame base
➤



Average image
➤



➤ Optical Diagnostics

- Visualization of transient flow and flame
 - **Schlieren** (Fastcam Photron High Speed CCD Camera Ultima 1024)
 - **OH Emission** Visualization (Fastcam Photron High Speed CCD Camera Intensified I2)



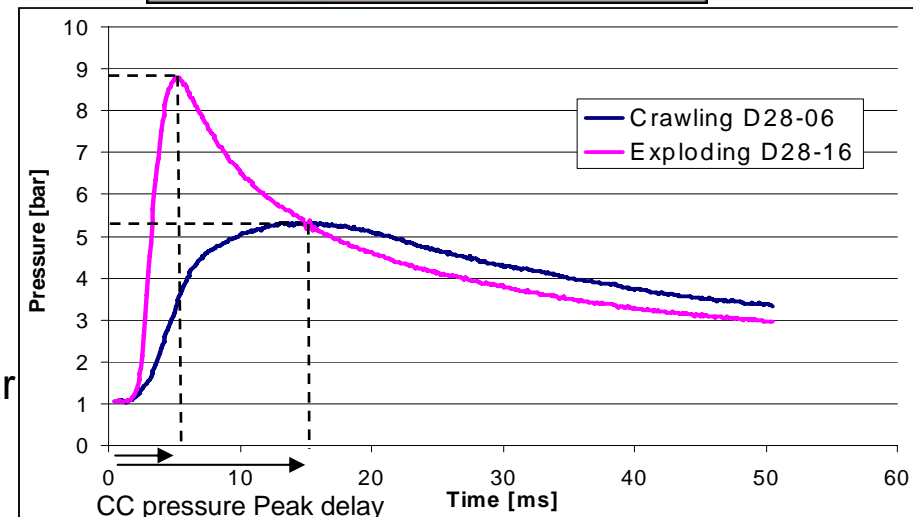
General Ignition Behaviour

- Two ignition types found for every configuration:
- **Crawling case, smooth ignition :**
 - Low OH emission
 - Flame crawling to the injector
 - Once anchored: the flame develops
 - Smooth pressure build-up with max pressure of 5.3 bar at 15 ms
- **Exploding case, hard ignition:**
 - High OH emission
 - Sudden consumption of all propellants inside the chamber
 - Blow down of the flame
 - Re-ignition at the injector
 - High and fast pressure peak: 8.8 bar at 5.5 ms



Crawling
(smooth ign.)

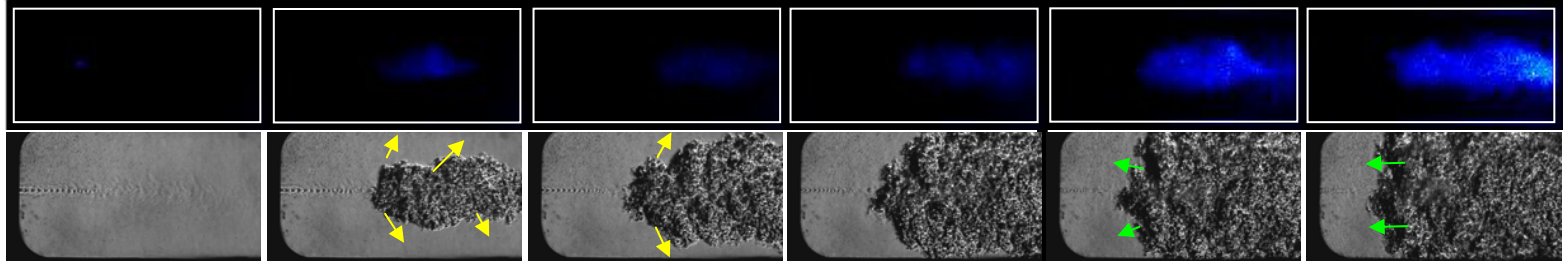
Exploding
(hard ign.)



Crawling Case

A21-12
OH images
 $\Delta t = 0.48 \text{ ms}$

Schlieren
 $\Delta t = 0.5 \text{ ms}$



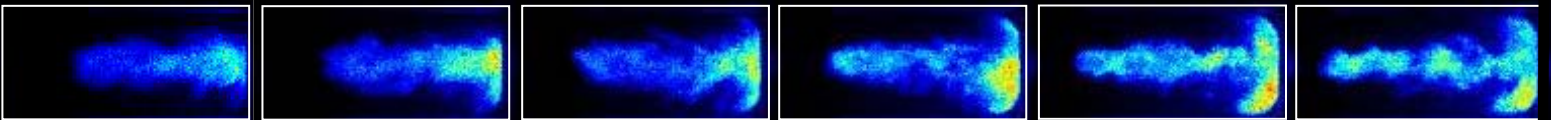
Phase 1: Move Downstream Phase: 0 ms -> ~1.5 ms

Flame kernel moves downstream (but flow modified in the whole chamber)

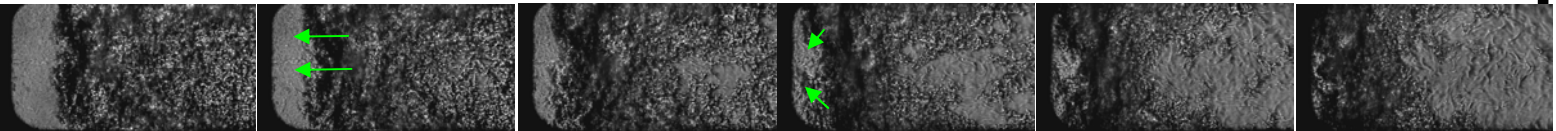
Phase 1

2

$t = 2.88 \rightarrow 5.28 \text{ ms}$



$t = 3.0 \rightarrow 5.5 \text{ ms}$



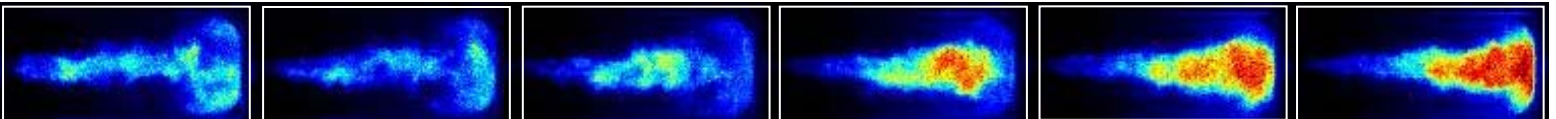
Phase 2: Expansion phase: ~ 1.5 ms -> ~ 5.5 ms

Flame develops in intensity and moves upstream to anchor the injector

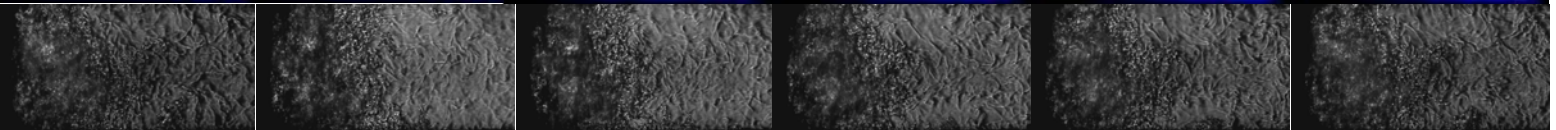
Phase 2

3

$t = 5.76 \rightarrow 8.16 \text{ ms}$



$t = 6.0 \rightarrow 8.5 \text{ ms}$



Phase 3: Flame development phase: ~ 5.5 ms -> steady

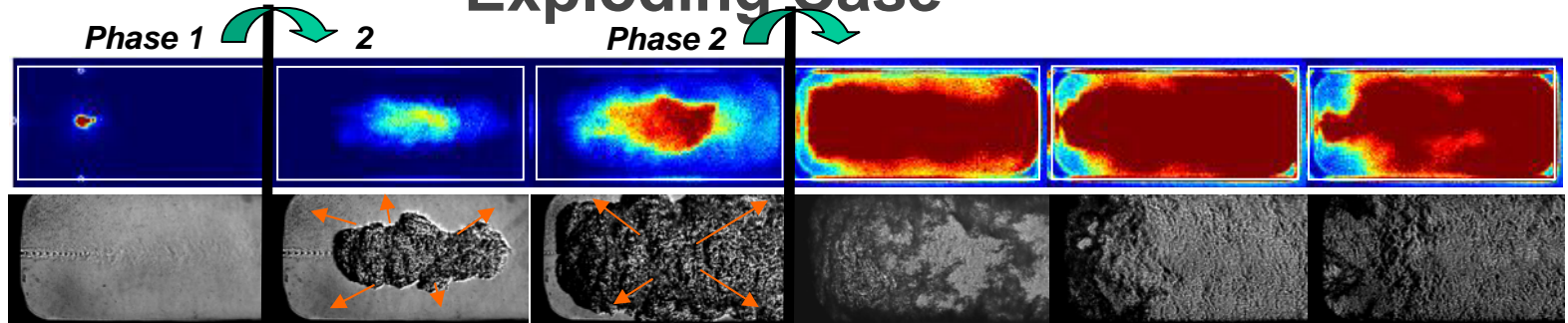
Flame is anchored to the injector lips and is develops up to the steady combustion (lifted flame or anchored)



Exploding Case

A21-12
OH images
 $\Delta t = 0.48 \text{ ms}$

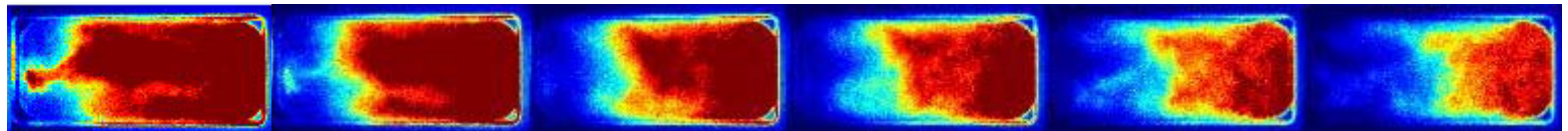
Schlieren
 $\Delta t = 0.5 \text{ ms}$



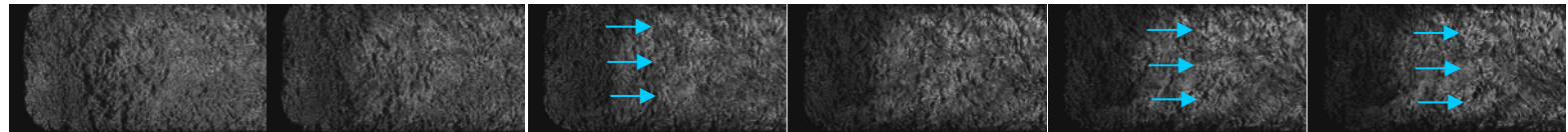
Phase 1 and 2: Blow down and Expansion phase : 0 ms -> ~ 3.5 ms

Sudden flame propagation consuming all the propellants accumulated in the chamber,

$t = 2.88 \rightarrow 5.28 \text{ ms}$



$t = 3.0 \rightarrow 5.5 \text{ ms}$



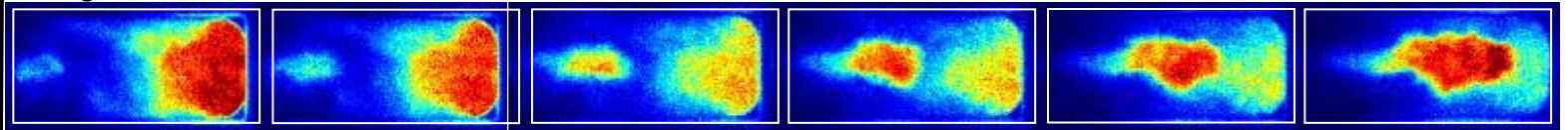
Blow out phase due to feed choke: ~3.5 ms -> 6.0 ms

Extinction of injection and blow down of the flame

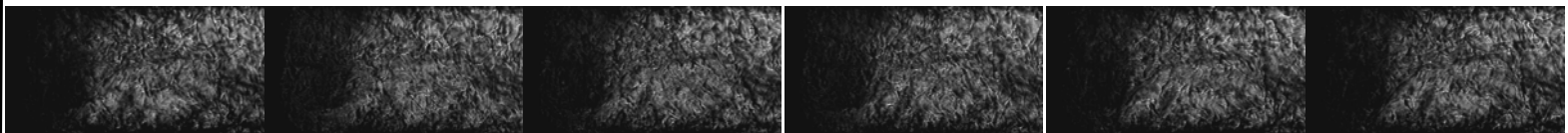
Phase

3

$t = 5.76 \rightarrow 8.16 \text{ ms}$



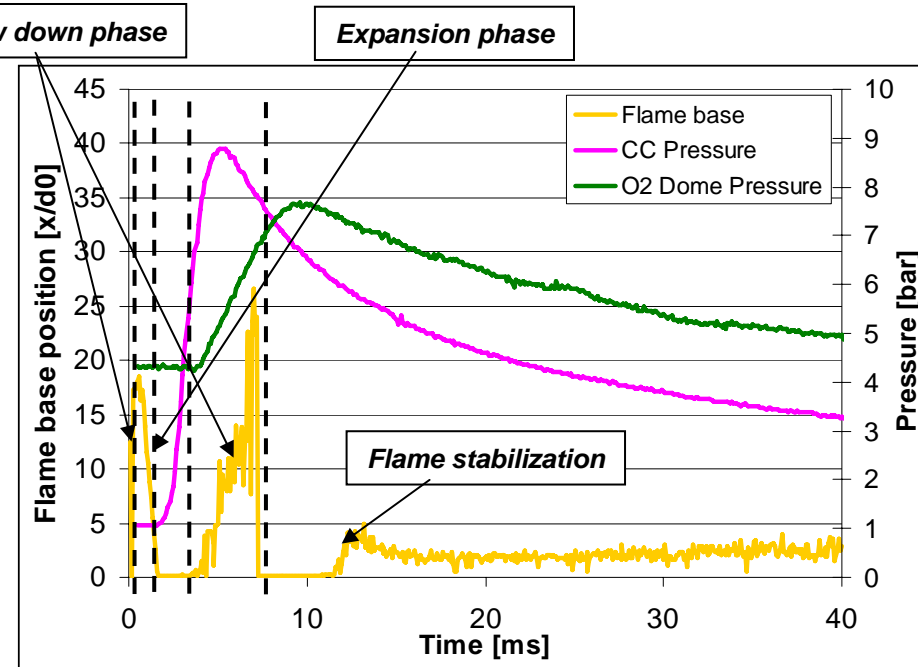
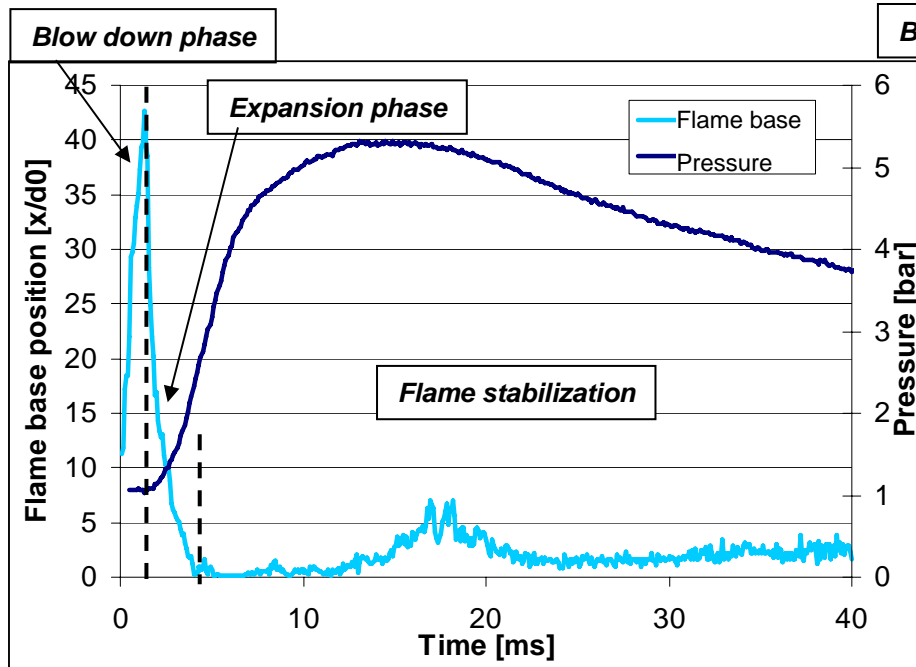
$t = 6.0 \rightarrow 8.5 \text{ ms}$



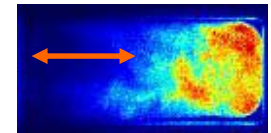
Phase 1, 2: Re-ignition phase with blow down: > 8.5 ms -> steady
Re-ignition of the flame at the injector lips, and flame developing



Flame base position

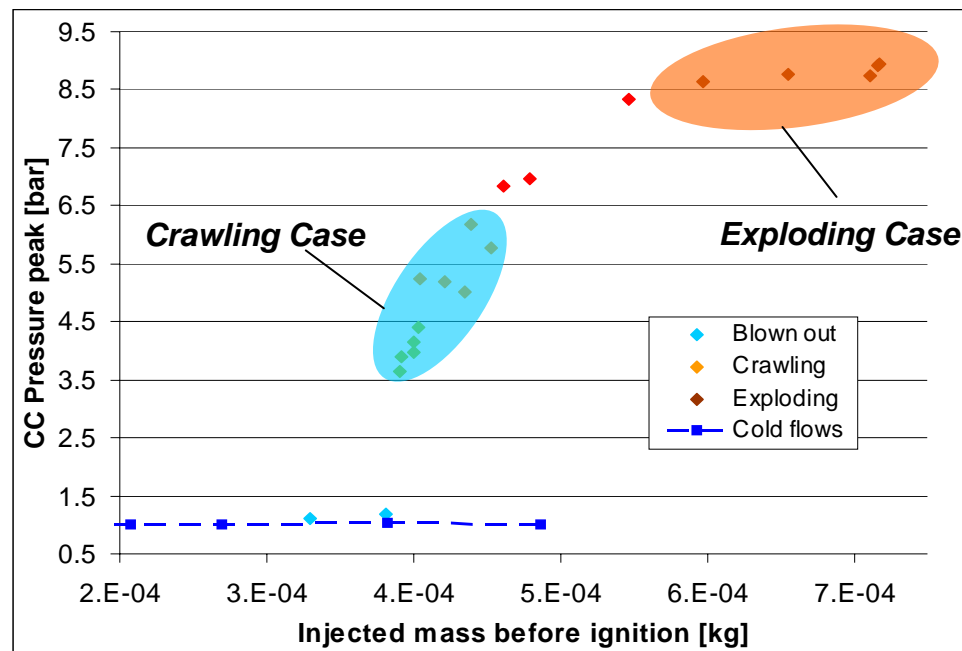


- Flame base position: Distance from the injector to the base of the flame
- Left: Flame anchoring without extinction of injection
- Right: Flame blown out because of the high CC pressure peak
 - Choking of oxygen injection
 - Re-ignition after pressure peak at the injector



Valve opening time

- Both type of ignition observed for every test cases
- Dependant of one parameter: the times of valve opening
- Earlier valves opening -> higher mass of reactants inside the chamber prior to ignition
 - Pressure peak higher
 - Change type of ignition -> crawling to exploding



- Injected mass = integration of the mass flow rate from the valve opening time to the ignition time

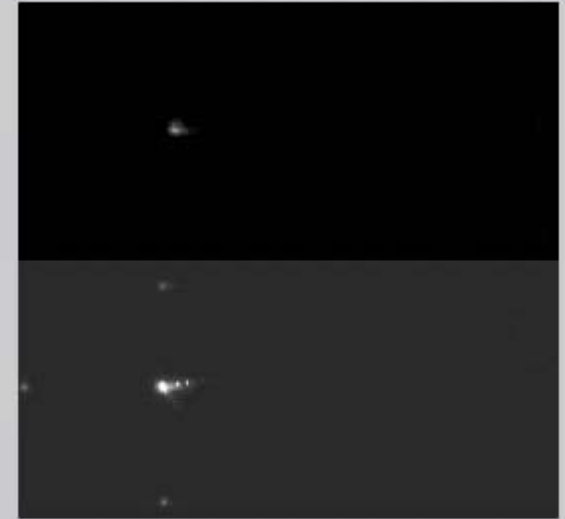
Influence of mass flow rate on ignition processes

(Test case C1/C2)

- Comparison with similar:
 - $P_c = 2.2$ bars
 - Same time of opening (same injected mass)
- Different mass flow rate:
 - Exit nozzle diameter: 6 & 4 mm
 - mass flow rate: 4.4 g/s & 2 g/s

C125_11
High mass flow

C226_16
Low mass flow

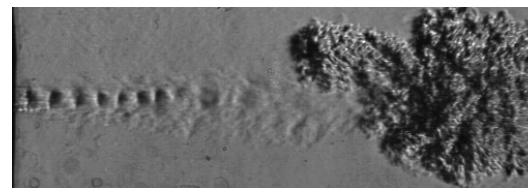
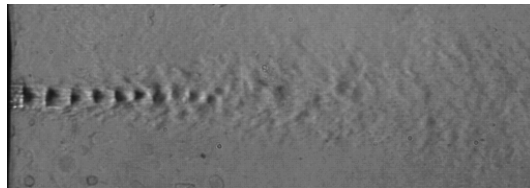


gcho060725_11_26_15_montage_OH.avi

t = 0.0 ms

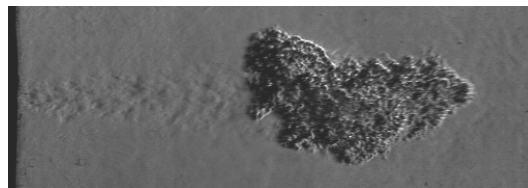
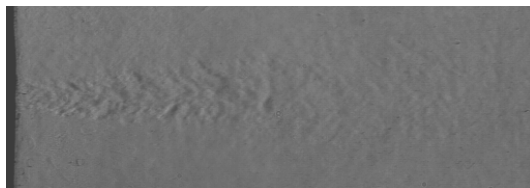
t = 0.5 ms

C125_11
High mass flow



sonic jet at the ignition time

C226_16
Low mass flow



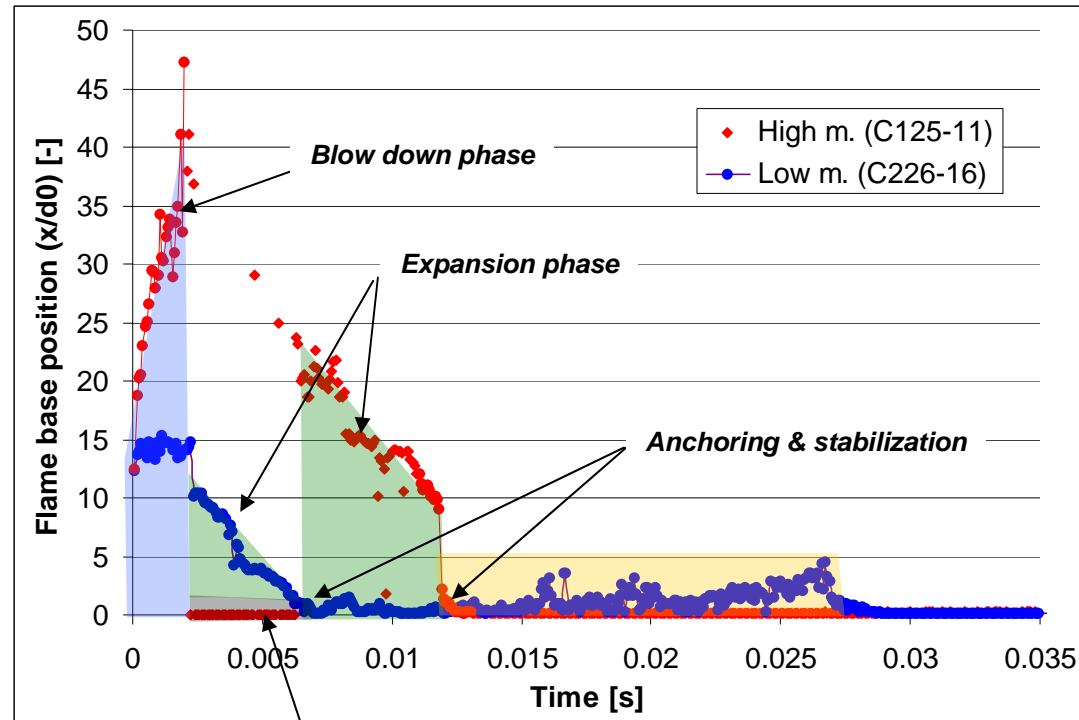
subsonic jet at the ignition time



Mass Flow Rate Influence on Ignition (Test cases C1/C2)

High mass flow case:

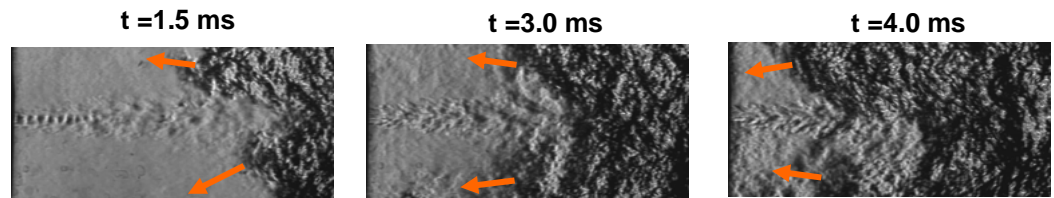
- Anchoring longer, due to high O_2 -injection velocity
- Flame stabilization faster, presumably Injection condition are less sensitive to the variations of chamber pressure
- Low intens. flame: almost no OH emission visible
 - Front of gradient density moving upstream
 - Loc. of flame reoccurrence indicates loc. of low intens. Flame at the end of CC



Three phases

- Blow down,
- Expansion &
- Stabilization found.

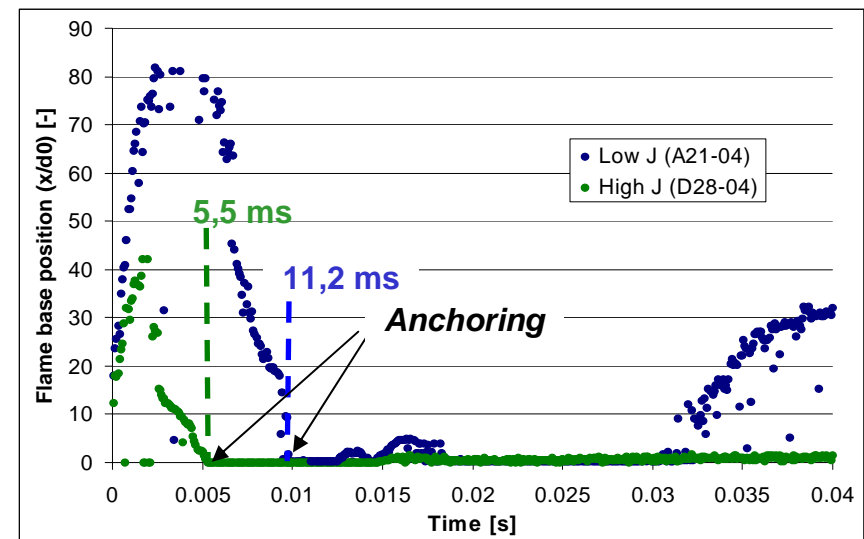
Depending on inj. cond. not every phase was equally temporal resolved.



Influence of J number

➤ Comparison of injection processes with similar injected mass prior to ignition but with different J numbers:

➤ $J = 0.03$ (case A) & 0.36 (case D)



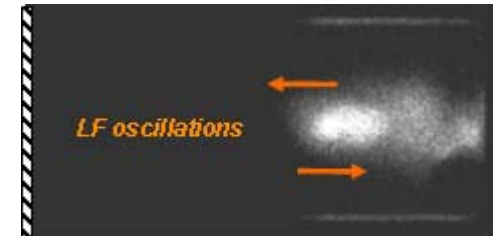
Flame Stabilization

CC Pressure Influence

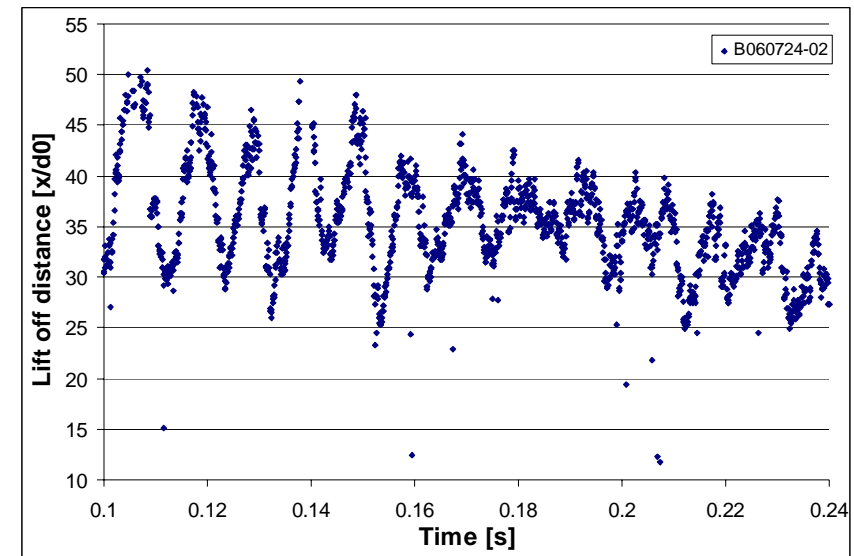
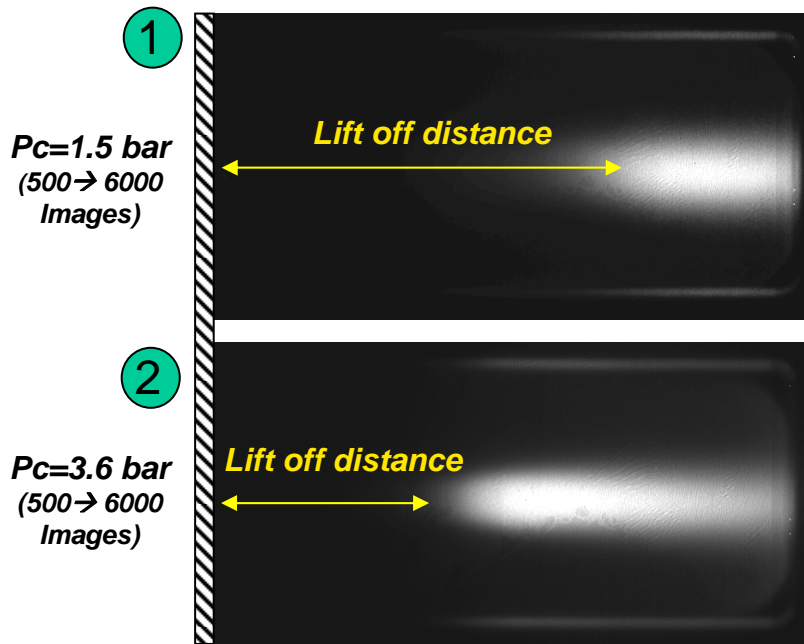
- Computation of the lift off distance on average image
- Higher chamber pressures lead to lower lift off distances:

- $P_c = 1.5 \text{ bar} \rightarrow X_{\text{Lift off}} \sim 30 d_0$

- $P_c = 3.6 \text{ bar} \rightarrow X_{\text{Lift off}} \sim 15 d_0$



→ Higher stationary chamber pressure stabilize the flame



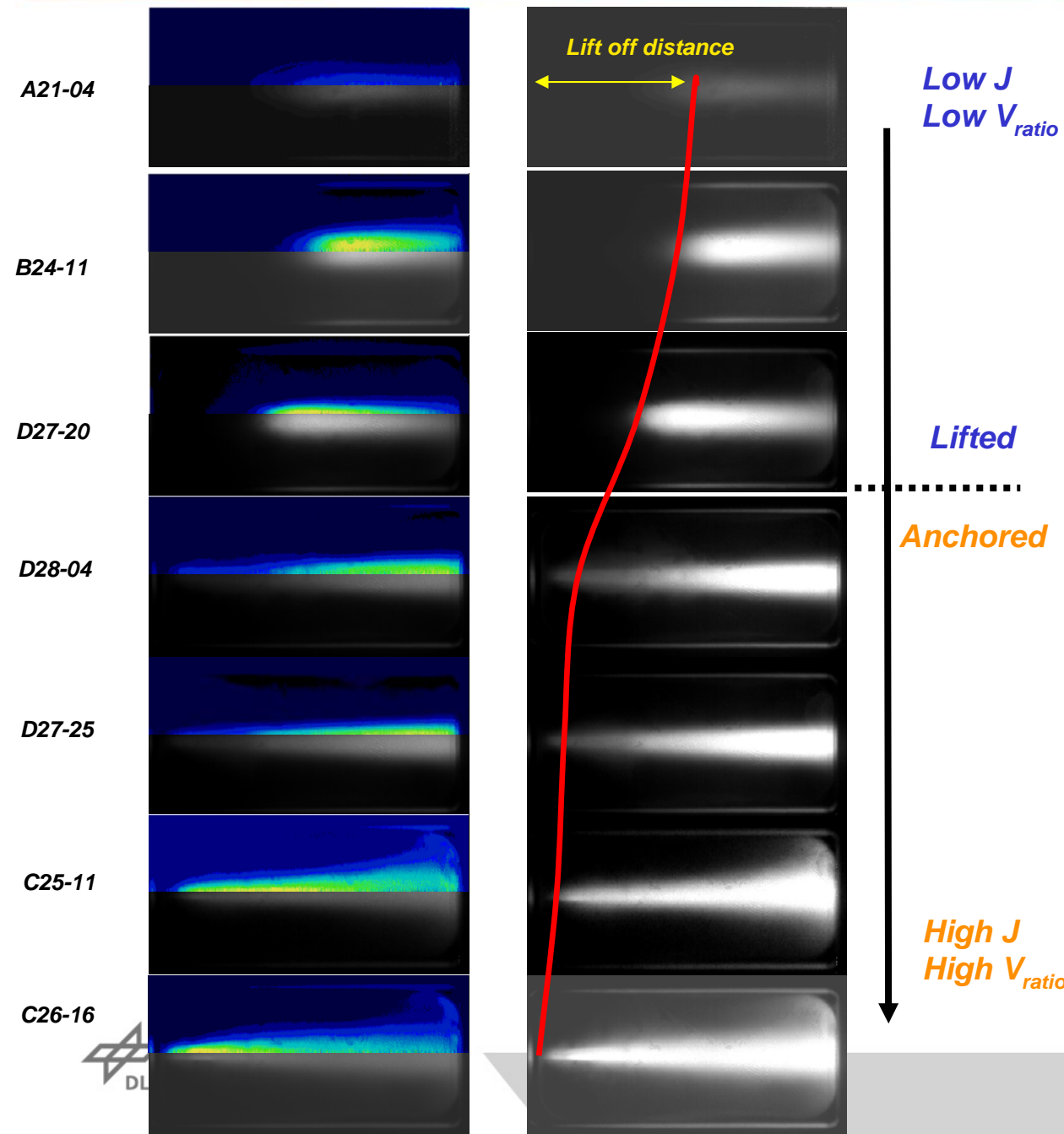
Flame Anchoring –

Influence of J & V ratios

Comparison of the average OH image during steady state combustion for every test

Test case	J [-]	Vratio [-]
A21-04	0.017	0.32
B24-11	0.134	0.54
D27-20	0.256	0.754
D28-04	0.292	0.802
D27-25	0.321	0.845
C1-25-11	1.72	1.52
C2-26-16	1.77	1.59

- Test case A, B: Lifted flame
- Test case C1, C2, D: Lifted flame & Anchored flames depending on the velocity ratio



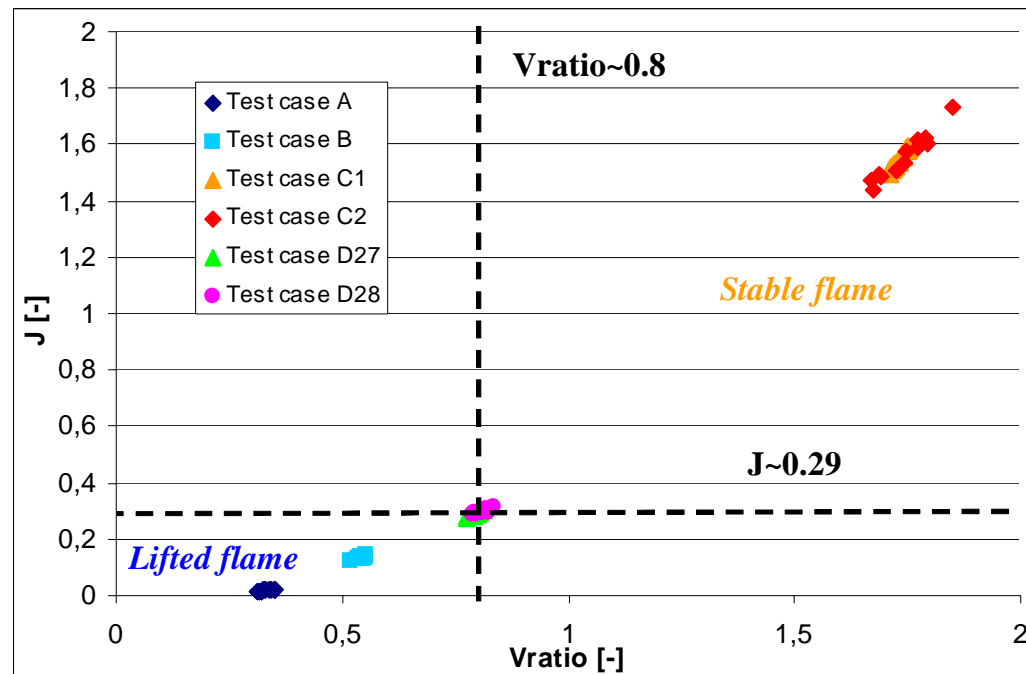
Flame Anchoring

Influence of the V ratio

- Critical value of velocity ratio to get a anchored or lifted flame:

$$V_{ratio} > \sim 0.80 \quad \Rightarrow \quad \text{Anchored Flame}$$

- With higher outer methane velocity, the local mixing inside the coaxial jet is better and the combustion enhanced, allowing thus the anchoring of the flame to the injector lips

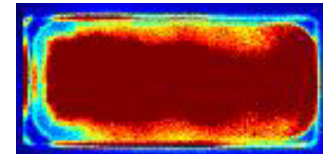
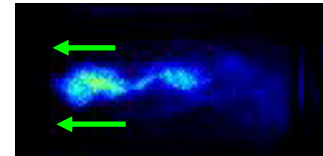


Conclusions

➡ Reliable ignition of a gaseous CH_4/O_2 coaxial jet ensured

- Influence of ignition time highlighted (injected mass before ignition)
- Three different ignitions phases (Blow down - expansion – stabilization)

Crawling ignition



Exploding ignition

➤ Influence of J number highlighted

- High J number:
Favors the flame anchoring because of a more efficient local mixing of the propellants

➡ Stabilization of the CH_4/O_2 flame to the injector lips ensured

- Chamber pressure increase favors the stabilization of the flame near the injector



Conclusions

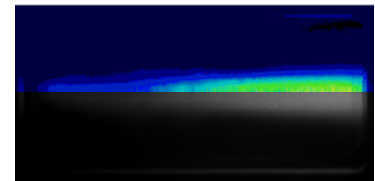
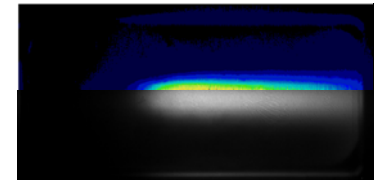
➡ Stabilisation of the CH₄/O₂ flame to the injector lips ensured

- Influence of the velocity ratio highlighted
 - For high V_{ratio} (> 0.8), the flame remains anchored

➡ Provide qualitative and quantitative for further CFD Computations

- Precision in boundary conditions ensured in terms of pressure and mass flow rate (calibration + shocked sonic nozzles)
- High temporal and spatial resolution quantitative data (pressure sensors: 10 kHz, OH imaging: 12 500 Hz)
- Importance of modeling the dome injector in CFD computation

Lifted flame



Anchored flame